

## LETTER TO THE EDITORS

### COMMENTS ON THE PAPER "THEORETICAL STUDY OF LAMINAR FILM CONDENSATION OF FLOWING VAPOUR"

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I WAS very interested to read the recent paper by I. G. Shekrladze and V. I. Gomelauri [1]. In a paper by J. D. Griffiths, J. W. Phillips and myself [2] we presented an analysis starting from similar assumptions, but in the general solution we included the shear stress arising from  $C_f^*$ . We did this because in our own experiments the vapour boundary layer was already fully turbulent at the leading edge of the condensing surface, and therefore we did not expect the effect of  $C_f^*$  to be negligible. Our analysis was more limited, however, in that we ignored the value  $U_s$  in the momentum stress  $j(U_\infty - U_s)$  at an early stage of the solution, and only considered the case of  $t_w = \text{constant}$ .

The analysis yielded an equation for the film thickness  $\delta$  at  $x$

$$(Sh) \left(\frac{\delta}{x}\right)^4 + (Dr) \left(\frac{\delta}{x}\right)^3 + (Re_v) \left(\frac{\delta}{x}\right)^2 = 1 \quad (1)$$

$Sh = \rho^2 g r x^3 / 4 \mu \lambda \Delta t$  accounts for the effect of gravity;  $Dr =$

$\rho \tau r x^2 / \mu \lambda \Delta t$  accounts for the effect of friction shear stress  $\tau = C_f^* \rho_v U_\infty^2 / 2$  which is additional to the momentum shear stress;  $Re_v = \rho U_\infty x / \mu$  is a two-phase Reynolds number which accounts for the momentum stress  $j(U_\infty - U_s) \approx j U_\infty$  (two-phase because it contains the properties  $\mu$  and  $\rho$  of the liquid but the velocity  $U_\infty$  of the vapour). Equation (1) can be solved for  $\delta$ , and the local Nusselt number found from  $Nu_x = x/\delta$ . It is also easy to show that the average Nusselt number  $Nu$  over a length  $x = \mathcal{L}$  is given by

$$Nu = \frac{4}{3}(Sh)\psi^3 + \frac{1}{2}(Dr)\psi^2 + \frac{1}{2}(Re_v)\psi \quad (2)$$

where  $\psi = \delta_{\mathcal{L}}/\mathcal{L}$ . Table 1 summarizes the results of film thickness  $\delta_{\mathcal{L}}$  at  $x = \mathcal{L}$ , and of average Nusselt number  $Nu = \alpha \mathcal{L} / \lambda$ , when some of the external forces acting on the film are neglected.

Equations (1) and (2) correspond to Nusselt's original simple theory which allowed only for gravity. Equations (5) and (6) are similar to Nusselt's solution in which he thought

Table 1

External forces acting on film	$\psi = \delta_{\mathcal{L}}/\mathcal{L}$	$Nu$
'General case'		
Gravity + Friction + Momentum	from equation (1)	from equation (2)
Gravity + Momentum	$\left[ \left\{ \left( \frac{Re_v}{8Sh} \right)^2 + \frac{1}{Sh} \right\}^{\frac{1}{2}} - \frac{Re_v}{8Sh} \right]^{\frac{1}{3}} \quad (3)$	$\left[ \left\{ \left( \frac{Re_v}{8Sh} \right)^2 + \frac{1}{Sh} \right\}^{\frac{1}{2}} - \frac{Re_v}{8Sh} \right]^{\frac{1}{3}} \times \left[ \frac{4}{3}(Sh) \left\{ \left( \frac{Re_v}{8Sh} \right)^2 + \frac{1}{Sh} \right\}^{\frac{1}{2}} + \frac{Re_v}{3} \right] \quad (4)$
Gravity + Friction	from $(Sh)\psi^4 + \frac{1}{3}(Dr)\psi^3 = 1 \quad (5)$	$\frac{4}{3}(Sh)\psi^3 + \frac{1}{2}(Dr)\psi^2 \quad (6)$
Momentum	$\left( \frac{4}{Re_v} \right)^{\frac{1}{3}} \quad (7)$	$(Re_v)^{\frac{1}{3}} \quad (8)$
Friction	$\left( \frac{3}{Dr} \right)^{\frac{1}{3}} \quad (9)$	$\frac{1}{2}(9Dr)^{\frac{1}{3}} \quad (10)$
Gravity	$\left( \frac{1}{Sh} \right)^{\frac{1}{3}} \quad (11)$	$\frac{4}{3}(Sh)^{\frac{1}{3}} \quad (12)$

that he had allowed for all the vapour drag, not realizing that the momentum drag term was mainly responsible for the shear stress on the film.

Our equation (8) corresponds to equation (9) of Shekri-ladze and Gomelaury and the latter can be put in the form

$$Nu = \left( \frac{Re_v}{1 + N} \right)^{\frac{1}{2}} \quad (13)$$

Since  $N \ll 1$  except for liquid metals, there is apparently good but not exact agreement between the two solutions.

Our equation (4) corresponds to equation (20) of Shekri-ladze and Gomelaury and the latter can be put in the form

$$Nu = (Re_v)^{\frac{1}{2}} \frac{\sqrt{2} \left[ 2 + \left( 1 + 64 \frac{Sh}{Re_v^2} \right)^{\frac{1}{2}} \right]}{3 \left[ 1 + \left( 1 + 64 \frac{Sh}{Re_v^2} \right)^{\frac{1}{2}} \right]^{\frac{1}{2}}} \quad (14)$$

There is no obvious way of showing whether this equation and equation (4) in Table 1 are identical or not, but sample calculations for typical particular situations give similar numerical results.

It is interesting to note that equation (14) for zero gravity,

i.e. for a horizontal plate for which  $Sh = 0$ , reduces to our equation (8) and not to equation (13). This suggests some inconsistency in their solution. It is also surprising that equations (13) and (14) do not contain  $U_s$ . The authors say that in deriving these equations they have used their equation (4), and not (3), but it is difficult to see at what point they have eliminated  $U_s$ . It is a pity that their deriva-tions and approximations, if any, are not even in outline.

#### REFERENCES

1. I. G. SHEKRILADZE and V. I. GOMELAURI, Theoretical study of laminar film condensation of flowing vapour, *Int. J. Heat Mass Transfer* **9**, 581-591 (1966).
2. Y. R. MAYHEW, D. J. GRIFFITHS and J. W. PHILLIPS, Effect of vapour drag on laminar film condensation on a vertical surface, Paper read at the Thermodynamics and Fluid Mechanics Convention, Liverpool April 1966, *Proc. Instn mech. Engrs* **180**, Part 3J (1965-66).

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